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PUBLIC WORKS CENTER PEARL HARBOR FLEET MOORINGS UNDERWATER INSPECTION PLAN

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OCEAN ENGINEERING
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by the Public Works Center, Pearl Harbor, HI. The inspection is scheduled to take place during the 1-21 may time frame.

CHESNAVFACENGCOM has designated an Engineer-in-Charge (EIC) to provide on-site technical guidance to Underwater Construction Team Two (UCT-2) divers who were tasked by CINCPACFLT message 210331Z August 1982 to perform the underwater portion of the inspection. In addition, the EIC will prepare the post inspection report which will include the results of the inspection and recommendations for required maintenance actions. (Section 1):

105 60

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PWC PEARL HARBOR UNDERWATER INSPECTION PLAN

1.0 BACKGROUND

As part of COMNAVFACENGCOM's Fleet Mooring Maintenance (FMM) Program, CHESNAV-FACENGCOM has been assigned the responsibility to conduct the underwater inspections of fleet moorings worldwide. This plan provides guidelines for the underwater inspection of 45 fleet moorings operated and maintained by the Public Works Center, Pearl Harbor, HI. The inspection is scheduled to take place during the 1 - 21 May time frame.

CHESNAVFACENGCOM has designated an Engineer-in-Charge (EIC) to provide on-site technical guidance to Underwater Construction Team Two (UCT-2) divers who were tasked by CINCPACFLT message 210331Z August 1982 to perform the underwater portion of the inspection. In addition, the EIC will prepare the post inspection report which will include the results of the inspection and recommendations for required maintenance actions.

2.0 PROJECT RESPONSIBILITIES

CHESNAVFACENGCOM will develop the FM underwater inspection plan, provide technical assistance to the dive team, prepare the required inspection forms, evaluate the observed inspection data, and report the results of the inspection to interested activities.

UCT-2 will provide sufficient divers to accomplish the inspection within the allotted time frame, gather and accurately report all required data, and ensure that the required amount of diving support material/equipment is available. In addition, UCT-2 divers will perform the underwater inspection in accordance with this plan and collect the data specified in paragraph 4.0.

The activity responsible for the moorings being inspected will provide logistics support as required by the Engineer-in-Charge and the UCT dive team.

3.0 GENERAL MOORING HISTORY

PWC Pearl Harbor currently operates and maintains 45 fleet moorings. The geographical positions of these moorings are shown in Figure 1. Although these moorings have been periodically removed,

A-/ Special or

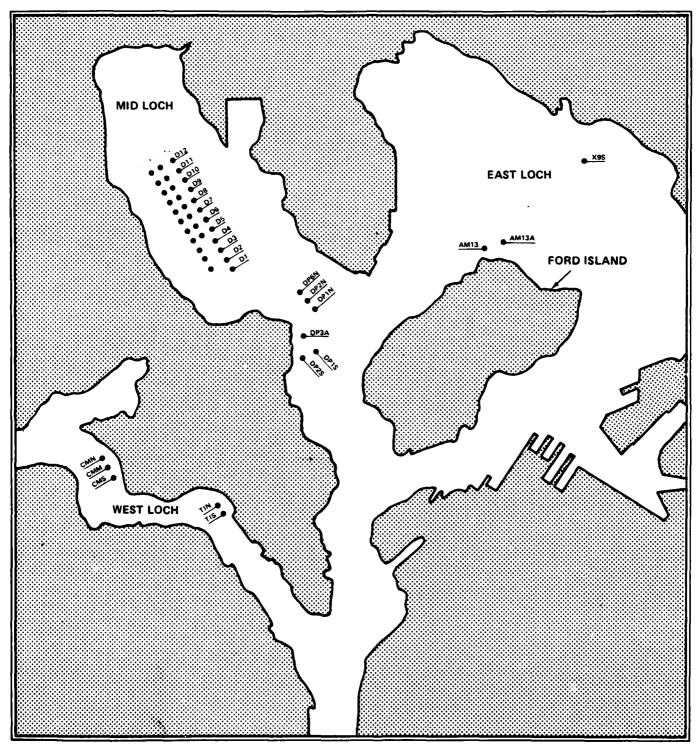


FIGURE 1. PEARL HARBOR FLEET MOORING LOCATION PLAN

inspected, repaired, overhauled, and downgraded as required, they have been in use for 30-35 years and much of the currently utilized mooring material is probably deteriorated and near the wear limit. The last underwater inspection of most of these moorings was conducted in November 1979 by CHESNAVFAC-ENGCOM with the assistance of divers from UCT-2.

The design of the PWC Pearl Harbor mooring systems and their mooring components vastly differ from the standard designs contained in DM-26. For example, the anchors for all of these systems are comprised of concrete clumps, concrete anchors, or combinations of both. In addition, the actual class of most of the moorings, based on results of the 1979 inspection, represents a substantial downgrade from the intended class indicated in PWC Pearl Harbor records (see Table 1). As-built data, schematics, and other historical data concerning these buoys are contained in Annex C.

4.0 INSPECTION PROCEDURES

4.1 <u>Inspection Objectives.</u> The purpose of mooring inspections is to determine the general physical condition of buoys and chain assemblies and, when possible, to verify or update existing as-built and maintenance records. Divers inspect only a portion of the submerged buoy hull and chain assemblies in order to compile a general description of the mooring's condition. The existence of fairly consistent measurements during this inspection provides a good indication of the mooring's overall condition. It should be kept in mind that periodic underwater inspections are intended as an expedient and relatively inexpensive supplement to accurate maintenance records. As such, they cannot fully substitute for a complete inspection involving recovery of the mooring and the measurement and evaluation of each component.

One of the more important parameters used to evaluate the condition of a mooring is chain wire diameter. After cleaning to bare metal, a selective sampling of the wire diameter of chain links and connecting hardware is taken in order to determine the amount of deterioration due to corrosion and wear. "Single Link" measurements are taken where chain is slack, and detect only corrosion loss. "Double Link" measurements, taken where two links connect under tension, detect the combined effects of corrosion and wear. Chain links and other components which measure 90% or greater of original wire diameter are considered to be in "good" condition; a measurement between 80% and 90% of original diameter is considered "fair" condition and is cause for the mooring to be downgraded in classification; any measurement less than 80% is considered "poor" and is cause for the mooring to be declared unsatisfactory for fleet use. Figure A-1 in Annex A depicts the proper method of taking both single and double link measurements.

TABLE 1. PWC PEARL HARBOR FLEET MOORINGS

Mooring No.	Mooring Class ⁽¹⁾ (Designed/Current)	Water Depth (Ft.)	Last Overhaul
AM13	C/D	31	?
AM13A	C/C	38	?
CMN	G/G	39	5/70
CMM	G/G	39	5/70
CMS	G/G	42	5/70
D1M	C/G	34	3/78
D2N	A/D	33	?
D2S	A/G	25	?
D3N	A/G	34	10/75
D3S	(2)	33	?
D4N	A/G	32	3/78
D4S	A/G	22	?
D5N	D/F	37	?
D5M	C/G	24	?
D5S	D/G	24	1/71
D6N	D/D	35	3/78
D6M	C/C	35	?
D6S	D/D	24	?
D7N	D/D	34	8/82
D7M	C/C	29	1/81
D7S	D/D	23	1/81
D8N	D/D	35	1/81
D8M	C/C	34	1/81
D8S	D/D	23	12/82
D9N	A/A	27	12/82
D9M	A/A	20	12/82
D9S	A/A	21	12/82
D10N	A/F	24	9/71
D10M	A/F	24	9/71
D10S	A/F	27	9/71
D11N	A/D	23	5/70
D11M	A/D	27	5/70
D11S	A/D	27	4/68
D12N	A/F	24	2/74
D12M	A/F	26	2/74
D12S	A/F	28	9/71
DP1N	A/A	40	3/82
DP1S	A/A	40	3/82
DP2N	C/C	36	3/82
DP2S	C/C	40	3/82
DP3A	C/F	12	1/72
DP6N	C/C	12	3/82
T1N	C/G	29	1/72
T1S	C/G	28	1/72
X9S	A/A	42	12/82

⁽¹⁾ Lower classification is a result of downgrading after 1979 underwater inspection.

⁽²⁾ Buoy broke loose from anchorage in 1979 and is currently on shore.

Standard underwater inspection procedures do not call for the inspection of any part of the mooring which is buried. Ground legs and risers are observed only to the point at which they become buried; no attempt is made to locate and inspect anchors or other mooring materials which are not readily visible.

- **4.2 Buoy.** The geographic position of each buoy will be verified. In order to accomplish this, a transit will be used to sight each buoy from known positions ashore.
- 4.2.1 <u>Buoy Upper Portion</u>. The buoy shall be observed to determine its general condition. The size of the buoy (diameter and height' should be recorded along with its freeboard. Physical damage such as holes, dents, or listing shall be described. If the buoy is fiberglass coated, the fiberglass should be inspected for cracks, wear, peeling, or rust-bleeding. A check will be made to see if the hatches have been fiberglassed over. If the buoy has not been fiberglassed, the paint will be checked for cracking, chipping, and peeling. Hatches, openings, and penetrations will be examined and broken parts and rust will be reported. Inspection check lists are contained in Annex B.

The buoy fenders and rubbing rails shall be checked for integrity and secure connection to the buoy.

Buoy top jewelry shall be identified and measured with calipers to find the overall outside dimensions and areas of most severe reduction in wire size. Methods for presetting calipers are contained in Annex A.

- 4.2.2 <u>Buoy Lower Portion</u>. Divers shall thoroughly inspect the buoy below the waterline. The thickness of marine growth shall be recorded, three one-foot-square areas shall be selected and cleared of growth without damaging the paint or fiberglass, and the condition of the paint or fiberglass will be noted. If the buoy is a riser-type with a hawse pipe, the presence and condition of the rubbing casting shall be recorded. If the buoy is cathodically protected, the condition, dimensions, and connection of anodes are to be noted. Then, electrical potential readings are to be taken with an underwater voltmeter at three locations on the buoy bottom.
- **4.2.3 Bottom Jewelry.** On each mooring, the jewelry connecting the buoy to the riser shall be identified and measured with calipers. As with the topside jewelry, the overall dimensions and the smallest wire size of each type of link or shackle will be recorded.

- A. The swivel and detachable links contained within the riser assembly shall be visually inspected and measured. As the divers swim down the riser, all chain links and other mooring hardware will be visually observed. Material suspected to be in worn or damaged condition will be investigated.
- 4.4 Ground Legs. Three consecutive double link measurements of each ground leg shall be taken at both ends and near the center of the visible portion of each ground leg. If the visible portion is longer than 90 feet, measurements shall be made every 45 feet. In those cases where the ground leg chain is slack and not in tension, three single link measurements shall be taken of each selected link as shown in Figure A-1 (Annex A). All connecting hardware including detachable links, anchor joining links, pear links, end links, swivels and shackles shall be identified and measured with calipers. Worn hardware and unusual chain joining practices shall be recorded and photographed.

The legs shall be labeled A, B, C, etc., clockwise from magnetic northand their orientation (determined by the diver's compass) sketched as in Figure 2.

4.5 Anchors. If an anchor is located, a pop float shall be attached to it so that the relative positions of the anchor from the mooring buoy can be observed from the surface. The anchor's position shall be recorded. The hardware connecting an anchor to its ground leg will be measured by calipers and the wire diameters recorded.

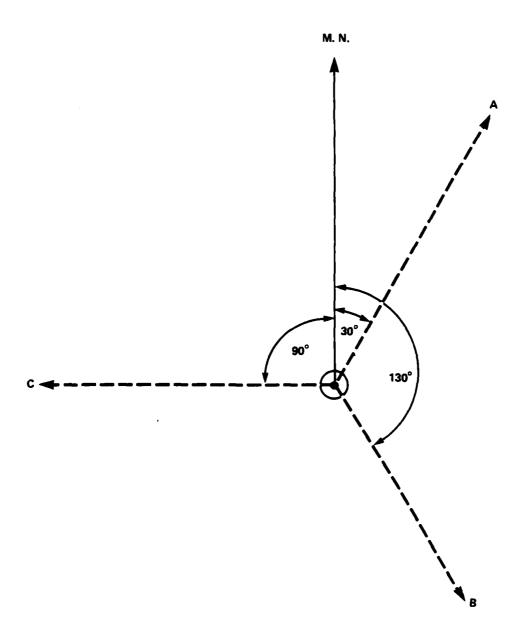
4.6 Photography

4.6.1 Topside. Topside photography and ashore photographs are the responsibility of the Engineer-in-Charge.

Photographs will be taken of each buoy showing its general condition. Photographs of the topside jewelry and damaged buoy components will be taken as deemed appropriate by the EIC.

Photographs will be taken of ashore spare mooring material inventories and construction equipment as deemed necessary.

4.6.2 <u>Underwater.</u> Underwater photography shall be the responsibility of the dive team. Buoy bottoms, bottom jewelry, worn links, swivels, ground rings, and other hardware shall be photographed wherever



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FIGURE 2. MAGNETIC BEARING OF GROUND LEGS

required to support material conditions and when environmentally feasible. Photographs shall include clear annotation as to the location of the hardware being photographed.

4.7 Cathodic Protection. Any moorings found to have cathodic protection will be inspected using the following procedures.

The underwater voltmeter will be used (after on-site calibration by the dive team) to probe the chain every 5 feet commencing with the buoy and bottom jewelry and continuing until the anchor is reached or the chain disappears into the bottom. All potential measurements will be recorded in the "Comments" column of Figure B-1. Before cleaning, divers will photograph each anode and record the thickness, type and accumulation of the coating. Several anodes should be brushed to remove the oxidation and the length, width and depth of the remaining zinc measured and photographed. Anodes in poor condition should be measured, reported and photographed.

5.0 DOCUMENTATION

The Engineer-in-Charge will document the inspection procedures used and record the data obtained by the dive team. He may require additional or alternative inspection procedures as deemed necessary during the course of the inspection. He will maintain a time log of events occurring during the inspection, and the master inspection form. In addition, the EIC must be prepared to debrief each diver, upon his return to the surface, in order to gain immediate knowledge of what the diver observed. The information obtained from the divers will be recorded, and this data will subsequently be the basis for the development of the moorings as-built configuration and for the preparation of the Fleet Mooring Inspection Report, which will contain the results of the inspection and recommendations for corrective maintenance actions.

While on site, the EIC will investigate the availability and cost of local mooring maintenance support. In addition he will conduct a cursory inspection of any on-shore Fleet Mooring Inventory (FMI) used for maintenance and repair or ready reserve. The type, size, quantity and general condition of the inventory shall be reported.

6.0 MEETINGS/BRIEFINGS

Upon arrival on site, the Engineer-in-Charge will conduct a pre-dive briefing to familiarize diving personnel with the mooring inspection procedures and to advise them of possible modifications to this

inspection plan. In addition, after approval by CHESDIV, the EIC will give a post-inspection debriefing to advise station personnel of the preliminary inspection findings.

7.0 LOGISTICS

- 7.1 <u>UCT TWO.</u> All arrangements for messing, berthing, and transportation of diver personnel, and the acquisition of a suitable dive platform/boat, will be the responsibility of UCT-2. In addition, the following equipment will be provided by the divers in support of this inspection:
 - All diving support equipment
 - Measuring aids
 - Inclinometer
 - 100' tape measures for use underwater
 - Scales 1, 2, and 3 feet with large numbers suitable for underwater photo documentation
 - Accurate depth gauges
 - Marker tags to relocate or mark chain links or accessories
 - Calipers (24 inch minimum)
 - Go/no-go guages
 - Survey equipment
 - Compass (diver's)
 - Survey buoys with line (pop floats)
 - Surveying transits for establishing mooring buoy locations.
 - Underwater voltmeters.
 - Two Underwater still cameras (35mm) with film (color and B & W) and flash with spare batteries
 - Cleaning equipment Hand tools including wire brushes, chipping hammers, and sharp chisels. Water blaster with water or hydraulic power supply and brush tool.

7.2 CHESNAVFACENGCOM. The CHESNAVFACENGCOM Engineer-in-Charge will provide the following:

- Inspection plan
- Data sheets and forms
- 35mm surface camera and film
- Drafting supplies, graph paper, scales
- Calculator
- Pre-dive briefing data
- DM-26

ANNEX A

MEASURING DEVICES AND THEIR USE

ANNEX A

1.0 MEASURING DEVICES AND THEIR USE

Tables A-1 and A-2 outline the 80 and 90 percent measurements for mooring components. These tables are based on the standard sizes of mooring material listed in DM-26 and can be used to preset calipers before measuring various items. For example, a class BB riser type mooring will require calipers set to 3.15" (90%) and 2.8" (80%) for single link measurements on the riser. These values are then doubled obtaining 6.3" (90%) and 5.6" (80%) for double link measurements on the riser. Similarly, for the ground legs, single link measurements of 2.25" (90%) and 2.0" (80%) are obtained from Table A-1. These values are also doubled to obtain 4.5" and 4.0" for double link measurements. For the ground ring, the 90% and 80% single link measurements are determined to be 5.85" and 5.2".

The preferred measuring devices, however, are back-to-back 80 and 90 percent "go-no go" gauges. These gauges simplify the diver's job in that, unlike calipers, they have to be damaged to be knocked out of adjustment underwater, and they normally do not have to be reset between dives. The locations for measuring chain links are shown in Figure A-1. Figure A-2 contains the drawings and data required to fabricate these gauges. Although these gauges provide a simpler way of sampling the wire size of chain links and some jewelry, the divers still have to carry calipers to measure ground rings and chain connecting links.

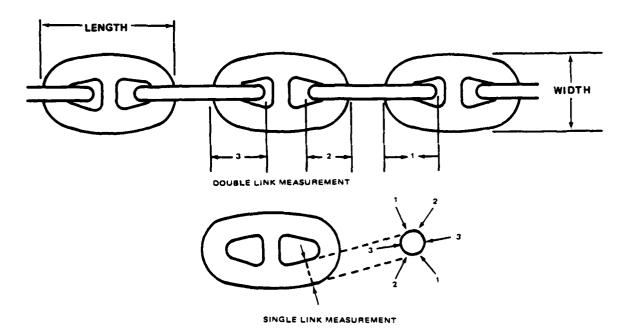


FIGURE A-1. LOCATIONS FOR TAKING CHAIN LINK MEASUREMENTS

(DOUBLE LINK MEASUREMENTS ARE OBTAINED BY MULTIPLYING SINGLE LINK MEASUREMENTS BY TWO) TABLE A-1. SINGLE LINK MEASUREMENTS FOR COMPONENTS OF RISER-TYPE MOORINGS

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P

		•	13,000	10.000	•	•	13.000	10.000	000.4	000.₽	2,000	300
Anchor	Stockless w/Stabilizer	25,000	20.000	000.81	30.000	25.000	\$0,000	10,000	13.000	9°,000	9,000	3,000
Tach le	1°V	2 3/4" type	25° type	?;" type	3" type	2 3/4" type	21. 170e	?;- type	2" Lype	1 3/4" Lype	lype	l. type
Ground Tackle	Chain	2.475 2.475 2.2	2.25 2.05 2.0	2.025 1.8	د ي ج	2.475 2.475 2.2	2.25	2.025 1.8	× 9.	1.575	1: 1.125 1.0	3/4 .675 .6
<u>ا</u>	Spider	4 3.6 2.7 3.2 2.4	4 3.6 2.7 3.6 2.7 3.2 2.4	4 3.6 2.7 3.6 2.7 3.2 2.4	•	•	•			•	•	•
Ground Ring	H I ng	6, 5.85 5.2	6°, 5.85 5.2	6's 5.85 5.2	6.2.4 6.6	5. 4.95	4.275	4.05 3.6	3.6	2.8 2.8 2.8	2.74 2.813 2.5	1 //B 1.648 1.5
	Ĭ	type		.; š	type	23/4- type		: Š	- 1,7pe	1 3/4°	1 1.pe	3/4- iype
Riser	Che in	1.6 3.2	2.5 2.5	2.5 8.5	- 	2.43 2.23 2.2	 	2.025 1.A		1,575	1.125	374 .675 .6
	1	type	3 1.ye	J.'.	tye	23/4-	 (70¢	7.5		1 3/4" Lype		3/4" Lype
Too of Buny	End Link	4', 3.285 2.92	3.544 3.544 3.15	3.15/16 3.544 3.15	3.375	3.038	3 1/8 2.813 2.5	2.813 2.813 2.5	 2.0.2 2.03	2.025 1.8	1.575	~. o. e.
100	f-Shackle	5 3/8 4.838 4.3	4 15/16 4.44 3.75	4.15/16 4.44 3.95	4 3/16 3.769 3.35	3.488 3.488	35 3,15 2.0	3 1/8 2.813 2.5	2 13/16 2.531 2.25	2 7/16 2.174 1.95	1.575	1 1/16 .956 .85
Percent	Remaining	5 5 S	228	ទិនខ	200	000	90 08 08	96. 8	888	0000	200	00.00
(18%)	Moor ing	A-A	:	÷	-	<	•	J	٠.	-	•	9

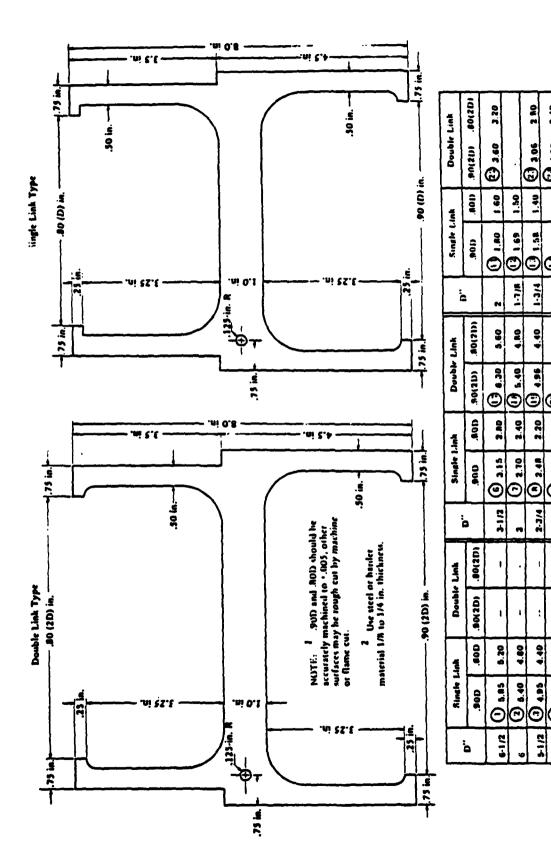
All measurement vary according to manufacturer, see IN-76 Assumes firm sand bottom Assumes cast steel chain

(DOUBLE LINK MEASUREMENTS ARE OBTAINED BY MULTIPLYING SINGLE LINK MEASUREMENTS BY TWO) TABLE A-2. SINGLE LINK MEASUREMENTS FOR COMPONENTS OF TELEPHONE-TYPE MOORINGS

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	171	•	13,000	10.000	•	•	13.000	10,000	900.
Anc hor '	Startless/Stabilizer	92,000	\$0.000	18,000	30,000	\$5.000	20.000	14,000	00,61
Tachle	(hain	2.3/4 2.405 2.2	2.25 2.95	2.025 1.8	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	2.374 2.275 2.2	% % %.0.	2. 2.025 1.8	8.1 1.6
Ground	Kil T (hain	2 1/4" type		7:- 1 vpe	J. tvpe	2 1/4- type	2'." 1 vpe	, , , , , , , , , , , , , , , , , , ,	1. Ne
lack le	Spider	3.6 2.7	3.2 2.7	3.6 2.7					
Brown to Crowned		t vre	, <u>}</u>	Y). yre	2 3/4" 1yre	- 1. July - 1. J	7: - 1ype	- C Also
Buote	3/1-Shactte	4 11/16 4.219 3.75	4.219	4.219	4.219	3.486	7. 15 7. 15	3 1/8 2.813 2.5	2.511 2.511 2.25
	Int All	type	÷ ,	type	type	y type	Type	1,70	y," type
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All measurements vary according to wandacturer, see PM-26 Assumes firm sand button Assumes cast steel chain



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FIGURE A-2. 10 PERCENT "GO-NO-GO" GAUGES

2.5

3.2 2.30

1.20

(<u>)</u>

1.3/4 1.1/2 1.174

+ 9.

2.20

2-3/4

4.40

\$1/2 4-172

(E) 4.50 £ 4.0%

(E) 2.25 E 2.03

2.1/2 2.174

9.40

(G) 7.20

5.20

3.60

\$ • **3 6**

Ē.

(C) 1.135

3.60

3. 2.00

ANNEX B

SAMPLE INSPECTION FORMS

Figures B-1 and B-2 depict two forms the EIC and divers may use to record measurements and as-built summations.

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FIGURE B.1

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MOORING NO.:	10.:	CLASS:			LOCATION	NO NO		LAT:			LONG:			
WATER DEPTH:	TH:	Ì	ANCHOR SIZE/TYPE	IZE/T)	/PE:			_ BUOY	BUOY TYPE:_					
BOTTOM TYPE:	PE: SAND	a	□ MUD	۳	CLAY		CORAL		Пвоск	Visibility_	lity	D = depth	Z	NI = not inspected, inaccessible
						CONDITION	TION							
₹ OO	COMPONENTS	ž	NEW	SIE	SINGLE LINK %	* ×	noa	DOUBLE LINK %	* *	a		COM	COMMENT	
				Š	- - - - - - - - - - - - - - - - - - -	8	÷	8	æ		_			
BUOY	BUOY HARDWARE													
										<u> </u>				
	NEAR BUOY													
RISER	MIDDLE													
	NEAR GRD RG													
GRC	GROUND RING							!						
	UPPER END													
CKCUND LEG	MIDDLE				ŀ									
¥.	ENTERS BOTTOM													
Civinoas	UPPER END													
LEG NO B	MIDDLE													
	ENTERS BOTTOM													
	UPPER END													
LEG NO C	MIDDLE													
	ENTERS BOTTOM													
	UPPER END													
LEG	MIDDLE													
	ENTERS BOTTOM													

DIVERS:

ENGINEER IN CHARGE:

DATE

FIGURE B-2 MOORING DATA SUMMARY FOR PREPARATION OF AS-BUILTS

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MOORING#	CLASS	LOCATION	DATE
BOTTOM TYPE	WATER DE	PTH MOORING	G CONDITION
ENGINEER-IN-CHARGE		DIVERS	
CONDITION		LEG C LENGTH EXPOSED LENGTH TYPE CHAIN LINK WIDTH WIRE DIAM.	
		LEG D LENGTH EXPOSED LENGTH TYPE CHAIN LINK WIDTH WIRE DIAM.	
GROUND RING LOC. OUTER DIAM. WIRE DIAM. CONDITION		RISER CONNECTIONS	
LEG A LENGTH EXPOSED LENGTH TYPE CHAIN LINK WIDTH WIRE DIAM.		OTHER	
LEG 8 LENGTH EXPOSED LENGTH TYPE CHAIN LINK WIDTH WIRE DIAM.			

ANNEX C

MOORING HISTORICAL DATA SUMMARY

(GFI PROVIDED BY PWC PEARL HARBOR)

LAT. COORD. (N) =
$$2i^{3}-22^{2}-30.5^{4}$$
 LONG. COORD. (W) = $157^{3}-57^{2}-38.6^{4}$

MRG ID = AMISA GENERAL LOC = Form Island (Nr. F-13) DES CLASS = C

DATE ESTAB = 1945 DEPTH = 36.0 ft. (ii) BOTTOM = Mud

LAT. COORD. (N) = $\frac{21-22-31.8}{}$ LONG. COORD. (W) = $\frac{157^{\circ}-57-34.3}{}$

BUOY TYPE = Riser-chain of hawsepipe SIZE = 12 0 x 6 hi

FENDER = IVeed FIBERGLASS COATING = No

CHAIN SIZE = 23/4."

SINKER = 1 WT. OF SINKER = 60,000 AF PADEYE SIZE = 2/4

OF ANCHORS = -

ANCHOR 1 WT = ____ PADEYE SIZE =

PADEYE SIZE = PADEYE SIZE = ANCHOR 3 WT = ____ ANCHOR 4 WT = ___

PADEYE SIZE = -

USAGE DURING PAST YEAR = 0 doys

TYPE OF SHIPS MOORED = CV

DATE OF LAST REPAIR/COST = 1977 / 124,050

DATE OF LAST OVERHAUL/COST = ?/?

DATE OF LAST UNDERWATER INSPECTION = CONDUCTED BY = CHESDIV (UCT TWO)

NEXT SCHED. REPAIR = 165

NEXT SCHED. OVERHAUL = 1437

DATE SHEET COMPILED = 8.82/MS

LAT. COORD. (N) =
$$21^{\circ}-21^{\circ}-26.6^{\circ}$$
 LONG. COORD. (W) = $157^{\circ}-59^{\circ}-34.3^{\circ}$

CHAIN SIZE =
$$2^{2/4}$$

SINKER =
$$\frac{1}{2}$$
 WT. OF SINKER = $\frac{34,000}{4}$ PADEYE SIZE = $\frac{2^2}{2}$ $\frac{1}{2}$

OF ANCHORS = 0

MRG ID = GMM GENERAL LOC = WEST Loch

DES CLASS = G

DATE ESTAB = 1943 DEPTH = 39.0 14. (MLW) BOTTOM = Mud

LAT. COORD. (N) = $\frac{2i^2-2i^2-24.6}{}$ LONG. COORD. (W) = $\frac{157^2-59-33.2}{}$

BUOY TYPE = Riser-chain N7 hawsepipe SIZE = 120x6 hi

FENDER = Rubber FIBERGLASS COATING = Yes

CHAIN SIZE = 23/4"

SINKER = $\frac{1}{24}$ WT. OF SINKER = $\frac{34,000}{4}$ PADEYE SIZE = $\frac{24}{4}$

OF ANCHORS = C

ANCHOR 1 WT = ANCHOR 2 WT =

PADEYE SIZE = PADEYE SIZE =

ANCHOR 3 WT = $^{\circ}$

PADEYE SIZE =

ANCHOR 4 WT = -

PADEYE SIZE = -

USAGE DURING PAST YEAR = 363 days

TYPE OF SHIPS MOORED = Lient careson

DATE OF LAST REPAIR/COST = 1977/\$2,750

DATE OF LAST OVERHAUL/COST = 5-70/?

DATE OF LAST UNDERWATER INSPECTION = 1979 CONDUCTED BY = CHESDIV (UCT THO)

NEXT SCHED. REPAIR = 1953

NEXT SCHED. OVERHAUL = 1985

DATE SHEET COMPILED = 8-82/MS

LAT. COORD. (N) =
$$21^{\circ}-21^{\prime}-22.9^{\circ}$$

LAT. COORD. (N) =
$$21^{\circ}-21^{\circ}-22.9^{\circ}$$
 LONG. COORD. (W) = $157^{\circ}-59^{\circ}-59.1^{\circ}$

CHAIN SIZE =
$$\frac{2\%4}{}$$

USAGE DURING PAST YEAR = 365 days

LAT. COORD. (N) =
$$\frac{21^{\circ}-27^{'}-19.2^{"}}{21^{\circ}-27^{\circ}-19.2^{"}}$$
 LONG. COORD. (W) = $\frac{157^{\circ}-59^{'}-00.6^{"}}{21^{\circ}-19.2^{"}}$

SINKER = 1 WT. OF SINKER =
$$\frac{60,000 \pm 1}{24}$$
 PADEYE SIZE = $\frac{214}{4}$

OF ANCHORS = -

DATE ESTAB = 1943 DEPTH = 33.0
$$ft./wwi$$
 BOTTOM = Mud
LAT. COORD. (N) = $21^{2}-22^{2}-23.9^{\circ}$ LONG. COORD. (W) = $157^{2}-59^{2}-01.0^{\circ}$

ANCHOR 1 WT =
$$60,000 \pm 0$$

ANCHOR 2 WT = $(100,0)$

ANCHOR 3 WT = $(100,0)$

ANCHOR 4 WT = $(100,0)$

PADEYE SIZE = $(100,0)$

PADEYE SIZE = $(100,0)$

PADEYE SIZE = $(100,0)$

LAT. COORD. (N) =
$$21-72-26.2$$
 LONG. COORD. (W) = $157-59-05.2$

SINKER = 1 WT. OF SINKER =
$$60,000$$
 PADEYE SIZE = $2\frac{1}{4}$

PADEYE SIZE =
$$\frac{2/4}{(Co_i)}$$

USAGE DURING PAST YEAR = 265 days

LAT. COORD. (N) =
$$21-22-27.0$$
" LONG. COORD. (W) = $157-59-03.6$ "

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13

SINKER =
$$\frac{1}{2}$$
 WT. OF SINKER = $\frac{66.000 \text{ ft}}{2}$ PADEYE SIZE = $\frac{2}{4}$

ANCHOR 1 WT =
$$\frac{2c_1c_2c_2}{2c_1c_2}$$
 PADEYE SIZE = $\frac{2}{2c_1c_2}$ ANCHOR 2 WT = $\frac{2c_1c_2c_2}{2c_1c_2}$ PADEYE SIZE = $\frac{2}{2c_1c_2}$ ANCHOR 3 WT = $\frac{2c_1c_2c_2}{2c_1c_2}$ PADEYE SIZE = $\frac{2}{2c_1c_2}$ PADEYE SIZE = $\frac{2}{2c_1c_2}$ PADEYE SIZE = $\frac{2}{2c_1c_2}$ PADEYE SIZE = $\frac{2}{2c_1c_2}$

ANCHOR 4 WT =
$$\frac{7D_0.7}{D_0.7}$$
 PADEYE SIZE = $\frac{7D_0.7}{D_0.7}$

LAT. COORD. (N) =
$$21^{\circ}-22^{\circ}-24.6^{\circ}$$
 LONG. COORD. (W) = $157^{\circ}-59^{\circ}-97.8^{\circ}$

B

ANCHOR 1 WT =
$$60,000$$
 #-

ANCHOR 2 WT = $(50.)$ PADEYE SIZE = $(70.)$ PADEYE SIZE = $(70.)$ PADEYE SIZE = $(50.)$ PADEYE SIZE = $(50.)$ PADEYE SIZE = $(50.)$ PADEYE SIZE = $(50.)$

USAGE DURING PAST YEAR =
$$\frac{C(x)}{?}$$

TYPE OF SHIPS MOORED = $\frac{?}{?}$

LAT. COORD. (N) =
$$21^{\circ}22^{\prime}-30.1^{\circ\prime\prime}$$
 LGNG. COORD. (W) = $157^{\circ}-59^{\prime}-06.2^{\prime\prime\prime}$

ANCHOR 1 WT =
$$60,0004$$
 PADEYE SIZE = $2/4.4$ PADEYE SIZE = (50) ANCHOR 3 WT = (50) PADEYE SIZE = (50) ANCHOR 4 WT = (50) PADEYE SIZE = (50)

LAT. COORD. (N) =
$$\frac{21^{\circ}-22^{\prime}-27.1^{\circ\prime\prime}}{27.1^{\circ\prime\prime}}$$
 LONG. COORD. (W) = $\frac{157^{\circ}-59^{\circ}-10.4^{\circ\prime\prime}}{27.1^{\circ\prime\prime}}$

SINKER =
$$\frac{1}{2}$$
 WT. OF SINKER = $\frac{60,006}{4}$ PADEYE SIZE = $\frac{2}{4}$

ANCHOR I WT =
$$\frac{60,000}{1000}$$
 PADEYE SIZE = $\frac{2}{4}$ PADEYE SIZE = $\frac{2}{4}$

LAT. COORD. (N) =
$$21^{2} - 22^{2} - 33.5^{\circ}$$
 LONG. COORD. (W) = $157^{2} - 54 - 08.6^{\circ}$

OF ANCHORS = __i

LAT. COORD. (N) =
$$21^{\circ}-22^{\prime}-31.8^{\circ}$$
 LONG. COORD. (W) = $157^{\circ}-59^{\prime}-10.9^{\circ}$

OF ANCHORS = 5

LAT. COORD. (N) =
$$21^{\circ}-72^{\circ}-30.3^{\circ}$$
 LONG. COORD. (W) = $157^{\circ}-59^{\circ}-13.0^{\circ}$

MRG ID = DGH GENERAL LOC = Middle Loch (ISMF) DES CLASS = D

DATE ESTAB = 1944 DEPTH = 35.0 ft./MLD) BOTTOM = Mud

LAT. COORD. (N) = 21-22-36.4 LONG. COORD. (W) = 57-59-11.4

BUOY TYPE = Ricer-chair of housepies SIZE = 12'0 x 6'hi

FENDER = Public FIBERGLASS COATING = Yes

CHAIN SIZE = 23/2.

SINKER = ___ WT. OF SINKER = ___ PADEYE SIZE = ___

OF ANCHORS = !

ANCHOR 1 WT = 60 ccc = PADEYE SIZE = 2/4 \$\phi\$
ANCHOR 2 WT = PADEYE SIZE = PADEYE SIZ

ANCHOR 3 WT = ___ PADEYE SIZE = __ ANCHOR 4 WT = ___ PADEYE SIZE = __

USAGE DURING PAST YEAR = 20 days

TYPE OF SHIPS MOORED = ? /OTEC / DD 948

DATE OF LAST REPAIR/COST = 1979/#780

DATE OF LAST OVERHAUL/COST = 5-78/?

DATE OF LAST UNDERWATER INSPECTION = 1979

CONDUCTED BY = CHESSIV (UCT TWO)

NEXT SCHED. REPAIR = 19.87

NEXT SCHED. OVERHAUL = 1964-

DATE SHEET COMPILED = 8-82/103

MRG ID = DG14 GENERAL LOC = Middle Loch (ISMF) DES CLASS = C

DATE ESTAB = 1950 DEPTH = 35.0 ft./MLV BOTTOM = Mud

LAT. COORD. (N) = $21^{\circ} 22^{\circ} 35.4^{\circ}$ LONG. COORD. (W) = $157^{\circ} - 59 - 13.4^{\circ}$

FENDER = Rubber FIBERGLASS COATING = Yes

CHAIN SIZE = 23/4"

SINKER = __ WT. OF SINKER = __ PADEYE SIZE = __

OF ANCHORS =

PADEYE SIZE = 2/4 0 PADEYE SIZE =

PADEYE SIZE =

ANCHOR 3 WT = ANCHOR 4 WT = -

PADEYE SIZE = 7

USAGE DURING PAST YEAR =

TYPE OF SHIPS MOORED = ? /OTEC/DC948

DATE OF LAST REPAIR/COST = 1976/82,000

DATE OF LAST OVERHAUL/COST = 7/3

DATE OF LAST UNDERWATER INSPECTION = CONDUCTED BY = CHESCY (UCT TWO)

NEXT SCHED. REPAIR = 1967

NEXT SCHED. OVERHAUL = 1064

DATE SHEET COMPILED = 6-85/MG

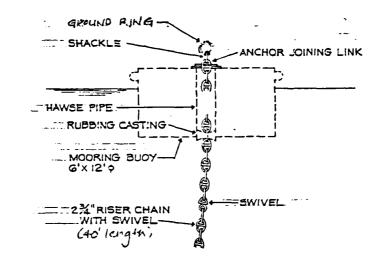
LAT. COORD. (N) =
$$21^{\circ}-22^{\prime}-33.4^{\circ}$$
 LONG. COORD. (W) = $157^{\circ}-59^{\prime}-15.5^{\circ}$

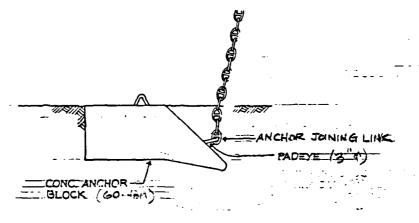
GENERAL LOC = Middle Lock_ (ZSMF)

DES CLASS = \mathcal{D}

LAT. COORD. (N) =
$$21^{\circ}$$
 22'-39.6"

LAT. COORD. (N) =
$$21^{\circ}$$
 22'-39.6" LONG. COORD. (W) = 157° -59'-13.9"





MOORING D7N

(8-85/MS)

LAT. COORD. (N) =
$$21^{\circ} 22' - 36.2''$$

PADEYE SIZE =
$$\frac{2/4}{4}$$
 APADEYE SIZE = $\frac{-}{4}$

LAT. COORD. (N) =
$$\frac{21^{\circ}-22^{\prime}-36.6^{\circ}}{21^{\circ}-22^{\prime}-36.6^{\circ}}$$
 LONG. COORD. (W) = $\frac{157^{\circ}-59^{\prime}-18.1^{\circ}}{21^{\circ}-18.1^{\circ}}$

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LAT. COORD. (N) =
$$21^{\circ}-22^{\circ}-47.7^{\circ}$$

LAT. COORD. (N) =
$$21^{\circ}-72^{\circ}-47.7^{\circ}$$
 LONG. COORD. (W) = $157^{\circ}-59^{\circ}-16.5^{\circ}$

CHAIN SIZE =
$$\frac{2^{3}4}{}$$

DATE OF LAST OVERHAUL/COST =
$$1-61/325,000$$
 (*)

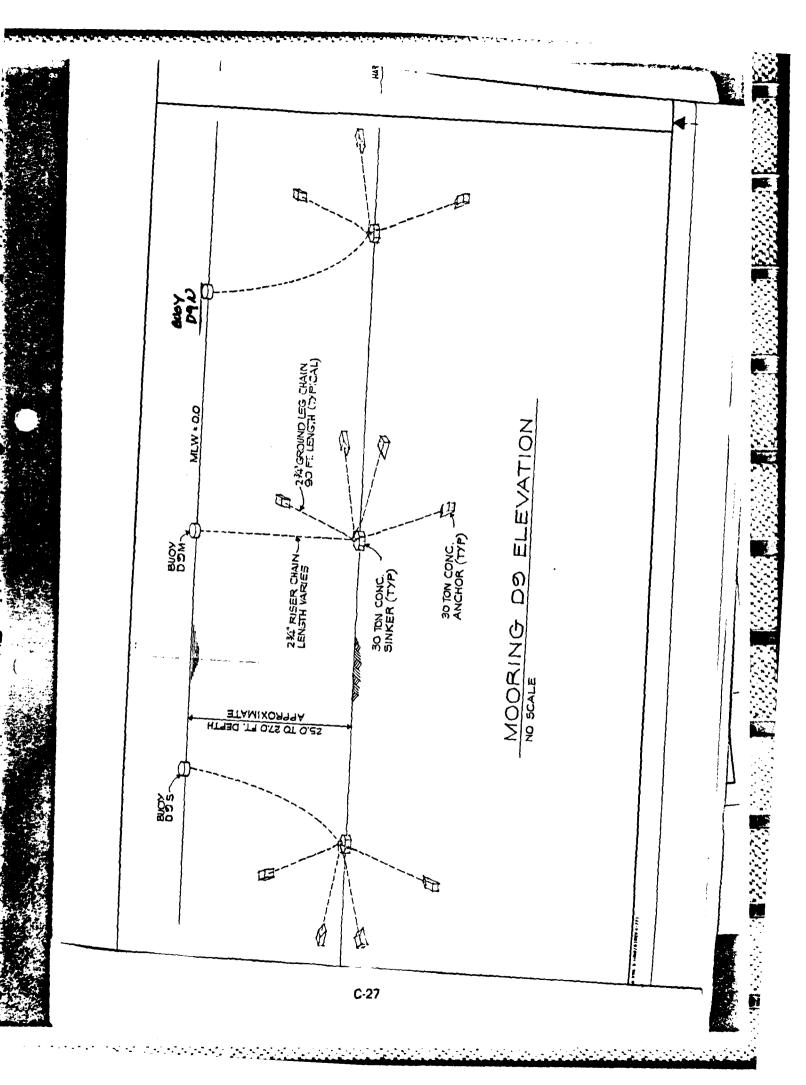
LAT. COORD. (N) =
$$21^{6}-22^{6}-41.2^{6}$$
 LONG. COORD. (W) = $157^{6}-59^{6}-18.6^{6}$

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LAT. COORD. (N) =
$$21^{2}-22^{2}-39.7^{2}$$
 LONG. COORD. (W) = $157^{2}-59^{2}-20.7^{2}$

(*) overhaul accomplished by Contr N62471-82-6-2164; Necessitated when mooring failed due to high winds during passage of Hurricane Iwa 11/23/82; This mooring done vice DIM of original contract.

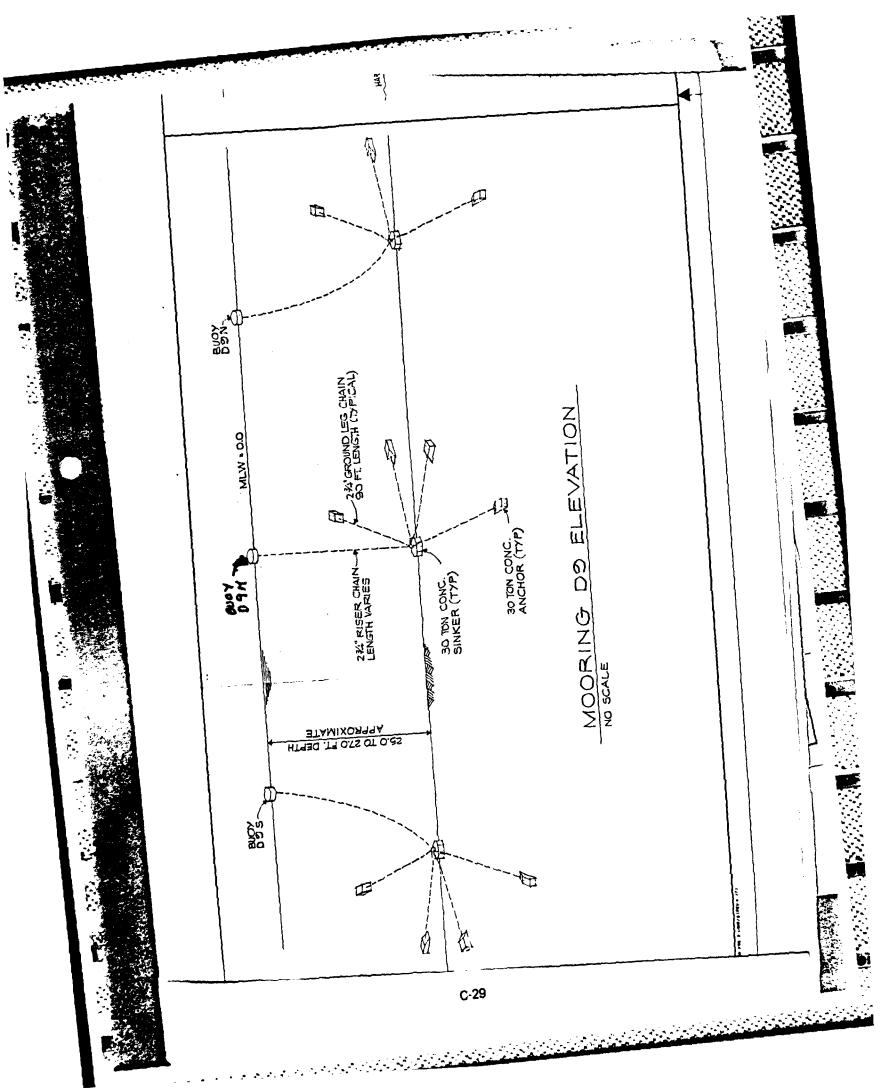
LAT. COORD. (N) =
$$21^{\circ} \times 2^{\circ} - 45.9^{\circ}$$
 LONG. COORD. (W) = $157^{\circ} - 59^{\circ} - 19.1^{\circ}$



LAT. COORD. (N) =
$$21^{\circ}-22^{\prime}-44.4^{\circ}$$
 LONG. COORD. (W) = $157^{\circ}-59^{\prime}-21.2^{\circ}$

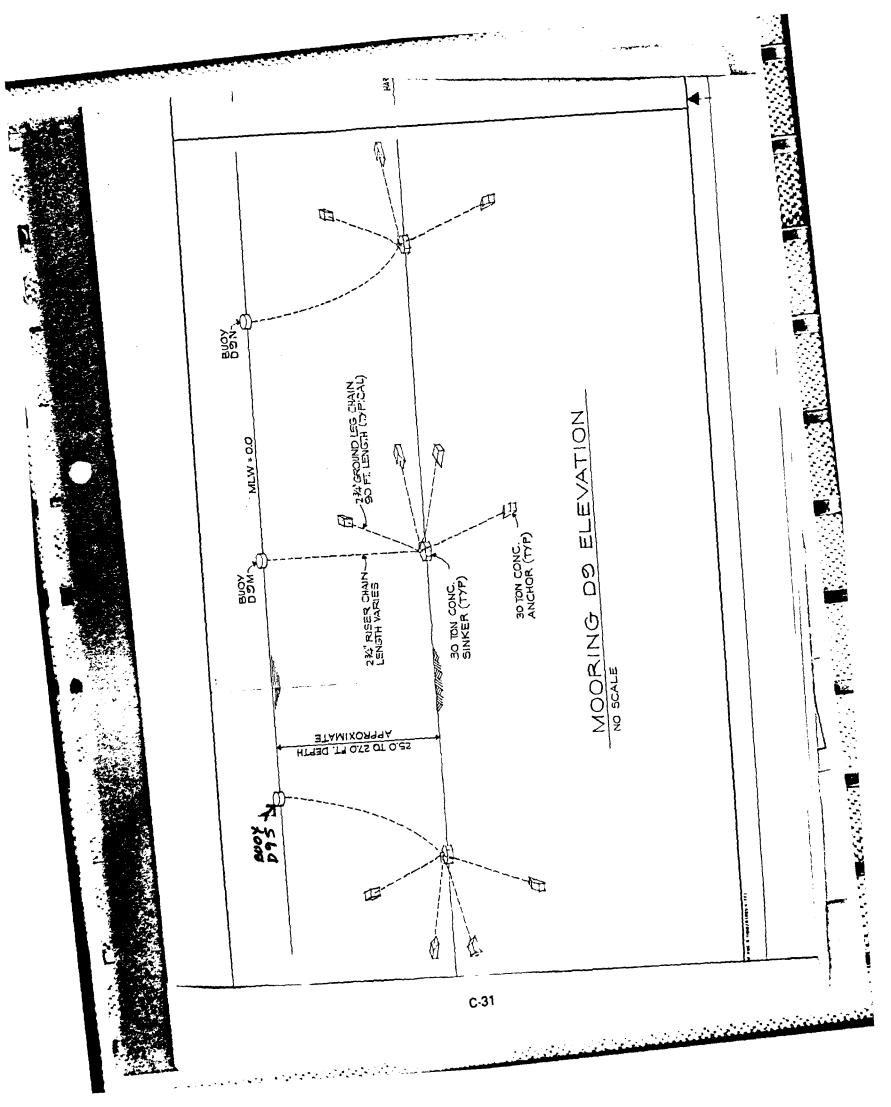
SINKER =
$$\frac{1}{24}$$
 WT. OF SINKER = $\frac{60,000 \pm 1}{24}$ PADEYE SIZE = $\frac{234}{4}$

(x) town-graded to class E after 1979 W/W Incp.



LAT. COORD. (N) =
$$21^{\circ}$$
 - 22° - 42.9° LONG. COORD. (W) = 157° - 59° - 23.3°

ANCHOR 3 WT =
$$\frac{(5a)}{(5a)}$$
 PADEYE SIZE = $\frac{(5a)}{(5a)}$ ANCHOR 4 WT = $\frac{(5a)}{(5a)}$ PADEYE SIZE = $\frac{(5a)}{(5a)}$



DES CLASS =
$$A(*)$$

LAT. COORD. (N) =
$$\frac{2! - 22! - 4.7.1}{}$$
 LONG. COORD. (W) = $\frac{157^{\circ} - 59! - 21.7}{}$

LONG. COORD. (W) =
$$157^{\circ}-59^{\circ}-21.7^{\circ}$$

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PADEYE SIZE =
$$\frac{2/4}{6}$$
 ϕ
PADEYE SIZE = $\frac{2}{6}$

ANCHOR 2 WT =
$$(5a.)$$

ANCHOR 3 WT = $(5a.)$

ANCHOR 4 WT =
$$\frac{(ba.)}{(ba.)}$$

USAGE DURING PAST YEAR = 365 days

LAT. COORD. (N) =
$$21^{2}-22-47.5^{\circ}$$
 LONG. COORD. (W) = $157^{\circ}-59-23.8^{\circ}$

CHAIN SIZE =
$$\frac{2^{3}/4}{4}$$

SINKER =
$$\frac{1}{24}$$
 WT. OF SINKER = $\frac{60,000}{4}$ PADEYE SIZE = $\frac{24}{4}$

DATE OF LAST OVERHAUL/COST =
$$\frac{9-71}{?}$$

LAT. COORD. (N) =
$$\frac{z_1^2 - 2z^2 - 46.0^{"}}{2.160}$$
 LONG. COORD. (W) = $\frac{157^2 - 59^2 - 25.9^{"}}{2.160}$

ANCHOR 1 WT =
$$60.000$$
 $4!$ PADEYE SIZE = 72.00 ANCHOR 2 WT = 60.00 PADEYE SIZE = 60.00 PADEYE SIZE = 60.00 ANCHOR 4 WT = 60.00 PADEYE SIZE = 60.00 PADEYE SIZE = 60.00

DATE OF LAST OVERHAUL/COST =
$$9-71/?$$

LAT. COORD. (N) =
$$21^{\circ} \cdot 22 - 52 \cdot 2^{\circ}$$
 LONG. COORD. (W) = $157^{\circ} \cdot 59 \cdot 24 \cdot 2^{\circ}$

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SINKER = 1 WT. OF SINKER =
$$60,000 \pm 9$$
 PADEYE SIZE = $2\frac{1}{2}$

LAT. COORD. (N) =
$$21^{6} \times 2^{2} - 56.7^{"}$$
 LONG. COORD. (W) = $157^{2} - 26.2^{"}$

SINKER = 1 WT. OF SINKER =
$$\frac{60,000}{4}$$
 PADEYE SIZE = $\frac{24.6}{4}$

LAT. COORD. (N) =
$$21^{6} 22^{6} - 49.2^{6}$$
 LONG. COORD. (W) = $157^{6} - 59^{6} - 28.4^{6}$

SINKER = 1 WT. OF SINKER =
$$\frac{60,000}{4!}$$
 PADEYE SIZE = $\frac{2/4}{4!}$

DATE OF LAST OVERHAUL/COST =
$$\frac{4-62}{?}$$

LAT. COORD. (N) =
$$21^{\frac{1}{22}}$$
 $55.8^{\frac{1}{2}}$ LONG. COORD. (W) = $157^{\frac{1}{2}}$ $26.8^{\frac{1}{2}}$

ANCHOR 1 WT =
$$\frac{60,000}{1000}$$
 PADEYE SIZE = $\frac{2/4}{400}$ ANCHOR 2 WT = $\frac{(00)}{1000}$ PADEYE SIZE = $\frac{(100)}{1000}$ ANCHOR 3 WT = $\frac{(00)}{1000}$ PADEYE SIZE = $\frac{(00)}{1000}$ PADEYE SIZE = $\frac{(00)}{1000}$

DATE OF LAST REPAIR/COST =
$$1977/42.750$$

DATE OF LAST OVERHAUL/COST =
$$\frac{2-74}{?}$$

MRG ID =
$$\frac{D1214}{}$$
 GENERAL LOC = $\frac{Middle Loch (ZCMF)}{}$ DES CLASS = $\frac{A}{/+}$

DATE ESTAB = 1950 DEPTH =
$$26.0 \text{ ft./MLW}$$
 BOTTOM = Mid
LAT. COORD. (N) = $21^{\circ}.22^{\circ}-53.8^{\circ}$ LONG. COORD. (W) = $157^{\circ}-59^{\circ}-28.9^{\circ}$

SINKER = WT. OF SINKER =
$$\frac{GC,CCO^{\frac{1}{2}}}{CCO^{\frac{1}{2}}}$$
 PADEYE SIZE = $\frac{2}{4}$ $\frac{4}{5}$

OF ANCHORS =
$$\frac{2}{}$$

LAT. COORD. (N) =
$$\frac{21-72-52.3}{}$$
 LONG. COORD. (W) = $\frac{157-57-31.0}{}$

SINKER =
$$\frac{1}{\sqrt{4}}$$
 WT. OF SINKER = $\frac{60,000^{24}}{\sqrt{4}}$ PADEYE SIZE = $\frac{2/4}{4}$

ANCHOR 1 WT =
$$GC_1CCC_1^{FC}$$
 PADEYE SIZE = $\frac{2A}{A}$ & PADEYE SIZE = $\frac{2A}{A}$ ANCHOR 3 WT = PADEYE SIZE = $\frac{2A}{A}$

DATE OF LAST OVERHAUL/COST =
$$\frac{9-71}{?}$$

DES CLASS =
$$A(r)$$

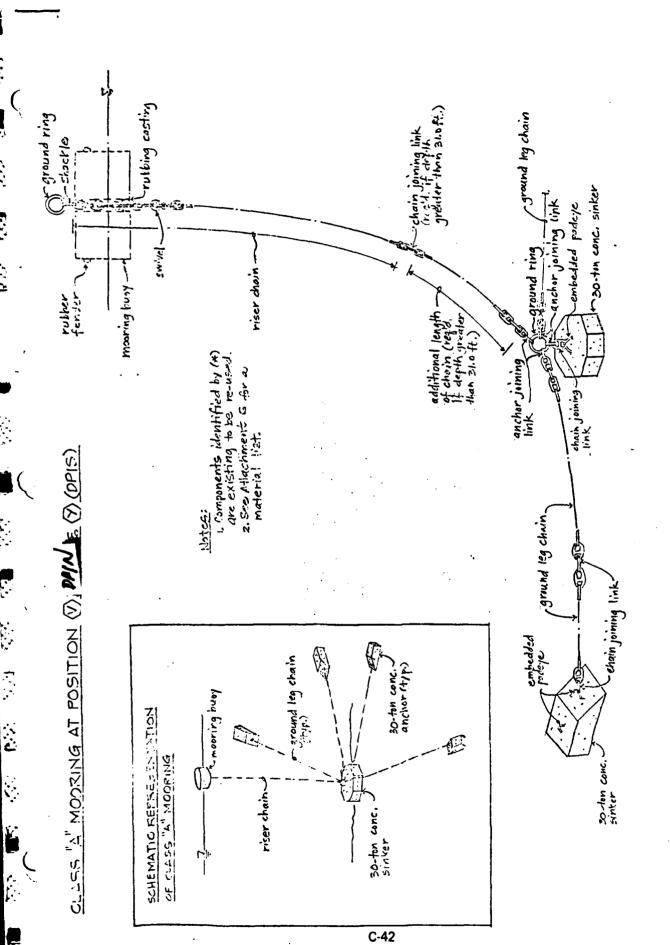
LAT. COORD. (N) =
$$21^{\circ}-22^{\circ}-12.0^{\circ}$$
 LONG. COORD. (W) = $157^{\circ}-56^{\circ}-33.6^{\circ}$

SINKER = 1 WT. OF SINKER =
$$\frac{60,000 \pm }{4}$$
 PADEYE SIZE = $\frac{24.4}{4}$

PADEYE SIZE =
$$\frac{z}{4}$$
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ANCHOR 1 WI =
$$(Co.)$$

ANCHOR 2 WT = $(Co.)$
ANCHOR 3 WT = $(Co.)$
ANCHOR 4 WT = $(Co.)$



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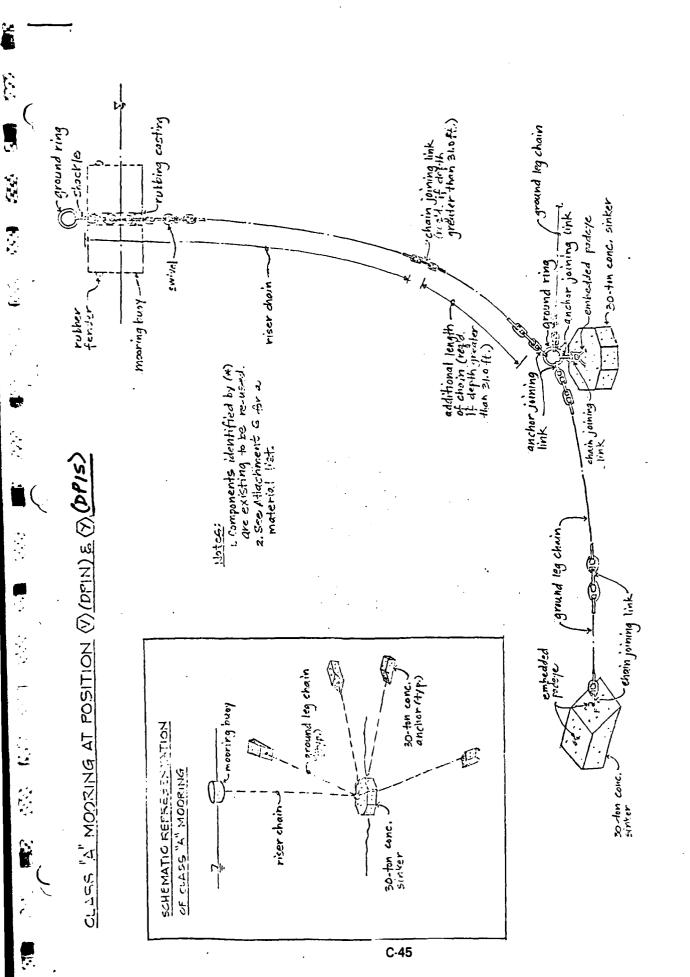
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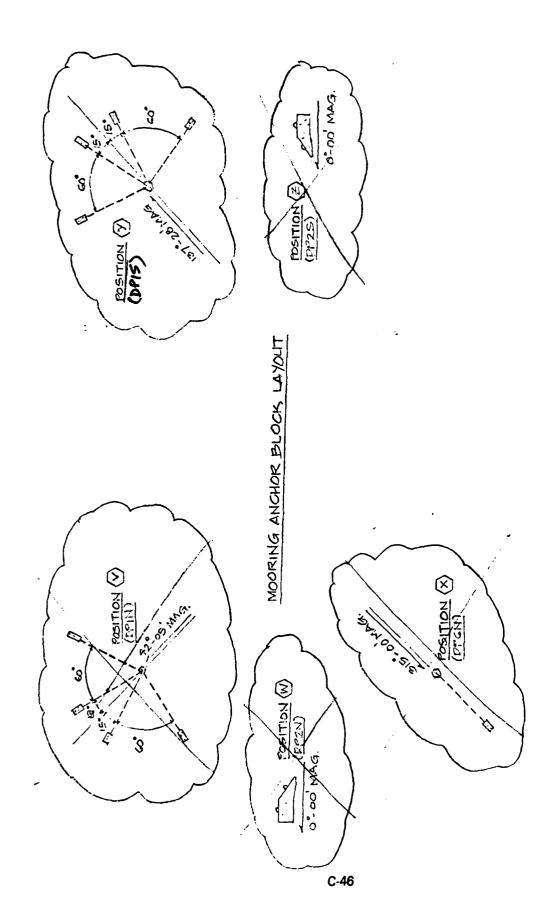
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LAT. COORD. (N) =
$$21^{\circ}-22^{\prime}-co.c^{\prime\prime}$$
 LONG. COORD. (W) = $157^{\circ}-58^{\prime}-35.7^{\prime\prime}$

CHAIN SIZE =
$$2.\frac{3}{2}$$
.





MRG ID = DPZN GENERAL LOC = Deperming Fac. DES CLASS = C

DATE ESTAB = FINITCH 1982 DEPTH = 36.0 H./MIN) BOTTOM = MUNC

LAT. COORD. (N) = $\frac{21^{2}-13.6^{\circ}}{157^{\circ}-58^{\circ}-35.8^{\circ}}$ LONG. COORD. (W) = $\frac{157^{\circ}-58^{\circ}-35.8^{\circ}}{157^{\circ}-58^{\circ}-35.8^{\circ}}$

BUOY TYPE = Ricei-chain of hawsepipe SIZE = 12 + x 6 hi

FENDER = Ribber FIBERGLASS COATING = Yes

CHAIN SIZE = 23/4"

SINKER = ___ WT. OF SINKER = ___ PADEYE SIZE = ___

OF ANCHORS = (

USAGE DURING PAST YEAR = 10 days

TYPE OF SHIPS MOORED = LINA / CO/CV

DATE OF LAST REPAIR/COST = ____

DATE OF LAST OVERHAUL/COST = Installation cost . \$11,000 (*)

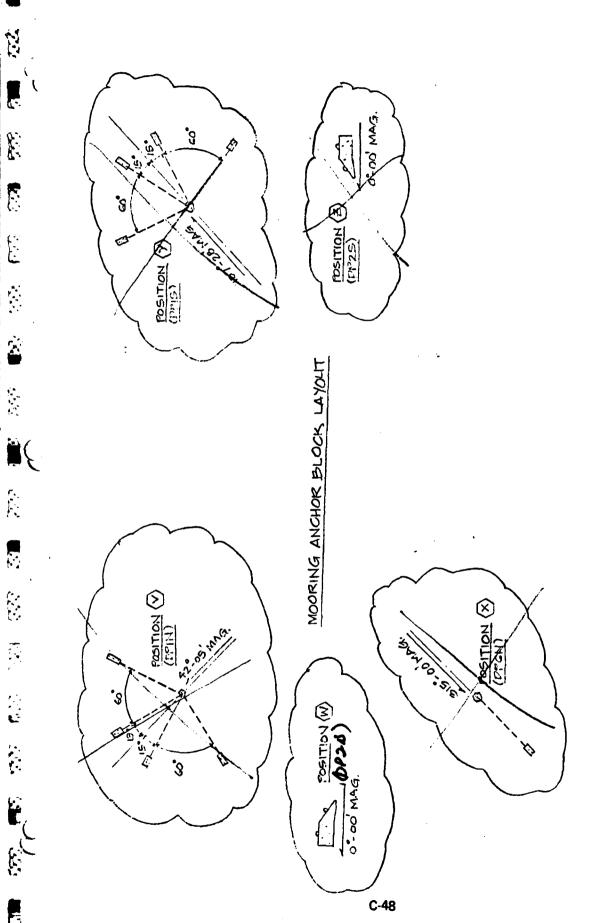
DATE OF LAST UNDERWATER INSPECTION = ____

NEXT SCHED. REPAIR = 1985

NEXT SCHED. OVERHAUL = 1987

DATE SHEET COMPILED = 8.82/MG

IN FUIC J.O. 190-6626, completed 262. PITIST flooding crane & diver services and full shop forces; super URBHIST accomplishments for Lital differming differ.



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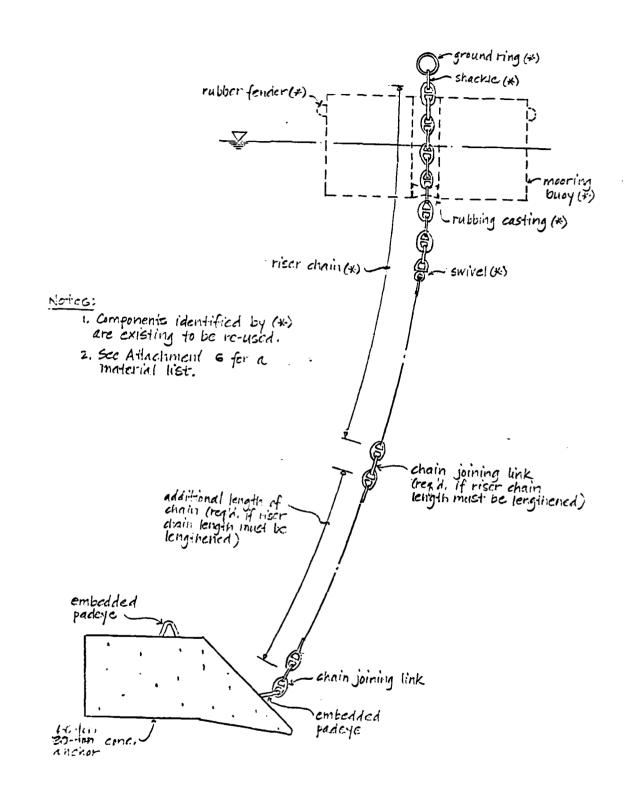
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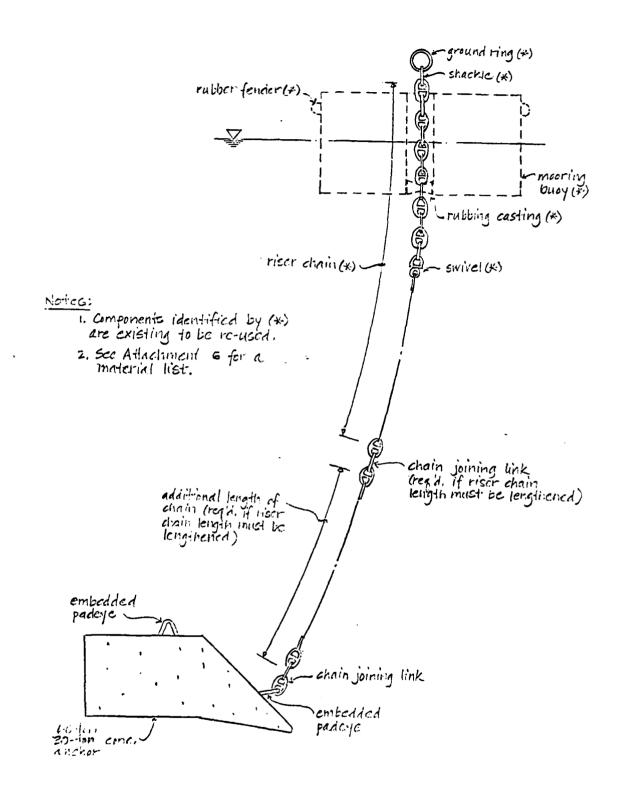
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CLASS "C" MOORING AT POSITION (W) (DPN) & (DF25)



CLASS "C" MOORING AT POSITION (W) (CF2N) & (E) (DP25)

C-52

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DATE ESTAB = 1948 DEPTH = 12.0
$$f(MUX)$$
 BOTTOM = Mud
LAT. COORD. (N) = 21-22-02.9" LONG. COORD. (W) = 157-58-39.1"

LAT. COORD. (N) =
$$21^{2}22 - 02.9$$
 LONG. COORD. (W) = $157^{2} - 58^{2} - 39.1$

DATE OF LAST REPAIR/COST =
$$\frac{1977/\$9,750}{}$$

DATE OF LAST OVERHAUL/COST = 1-72/?

MRG ID = UPGN GENERAL LOC = Deperming Fac.

DES CLASS = C

DATE ESTAB = 1943

DEPTH = 12.0 f(, (MILLY) BOTTOM = MUD

LAT. COORD. (N) = $2!^{6} 22!^{2} - 12.8"$ LONG. COORD. (W) = $157^{2} - 56!^{2} - 36.6"$

BUOY TYPE = Ricon chain of hawsopipe SIZE = 12 0 x 6 hi

FENDER = FILE FIBERGLASS COATING = YES

CHAIN SIZE = 23/4"

SINKER = $\frac{1}{4}$ WT. OF SINKER = $\frac{66,000}{4}$ PADEYE SIZE = $\frac{2}{4}$

OF ANCHORS = (4.)

ANCHOR 1 WT = 60,000 #

PADEYE SIZE = 2./4. 4 PADEYE SIZE =

ANCHOR 2 WT = ANCHOR 3 WT =

PADEYE SIZE =

ANCHOR 4 WT = $\overline{}$

PADEYE SIZE = 1

USAGE DURING PAST YEAR = 10 days

TYPE OF SHIPS MOORED = LHA/CC/CV

DATE OF LAST REPAIR/COST = 1977/ 44,050

DATE OF LAST OVERHAUL/COST = Installation cost = #(1,000(**)

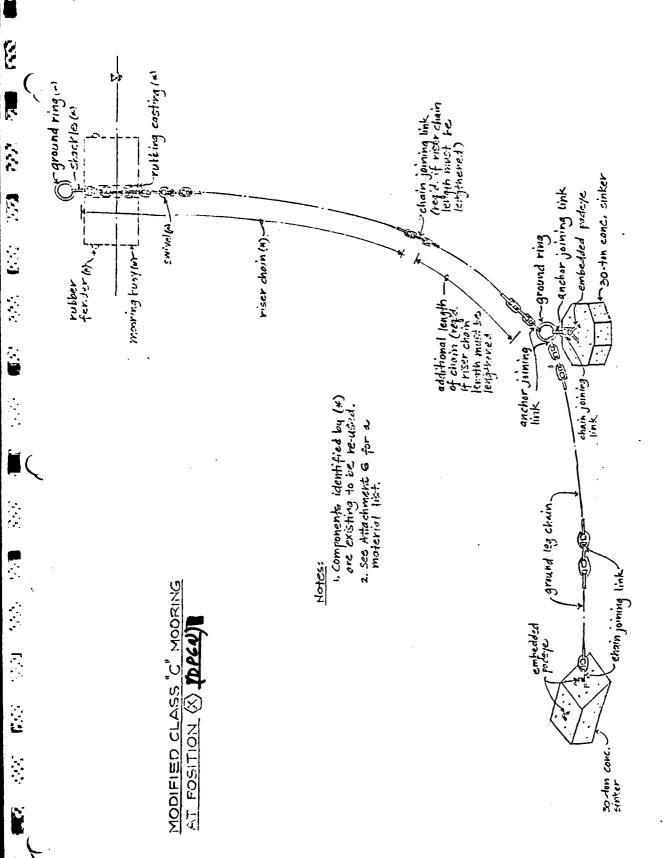
DATE OF LAST UNDERWATER INSPECTION = CONDUCTED BY = CHESDIV (UCT TWA)

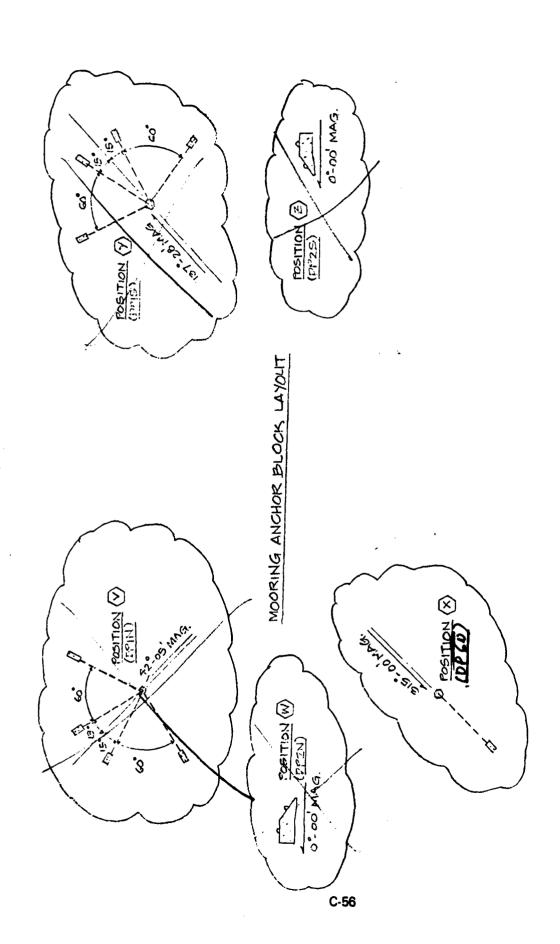
NEXT SCHED. REPAIR = 1985

NEXT SCHED. OVERHAUL = 1987

DATE SHEET COMPILED = 8-82/MS

- (*) This class C mooring has I sinker & I ground leg as directed by Eccermina hacility.
- (**) FUC J.D. 170-6626, completed 3/B2; PHNSY floating crane & diver services and FUC shop forces; sufer upself accomplishment for LHA deferming 4/62,





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LAT. COORD. (N) =
$$21^{\circ}21^{\circ}-13.5^{\circ}$$
 LONG. COORD. (W) = $157^{\circ}-58^{\circ}-59.7^{\circ}$

PADEYE SIZE =
$$\frac{z/4}{\phi}$$
PADEYE SIZE = $\frac{z}{\phi}$

USAGE DURING PAST YEAR = 10 days

DATE ESTAB =
$$\frac{1957}{1957}$$
 DEPTH = $\frac{28.C + \frac{1}{2}}{1957}$ BOTTOM = $\frac{Muq}{1957}$ LONG. COORD. (W) = $\frac{157^{\circ} - 59^{\frac{1}{2}}}{1957}$ OO.7"

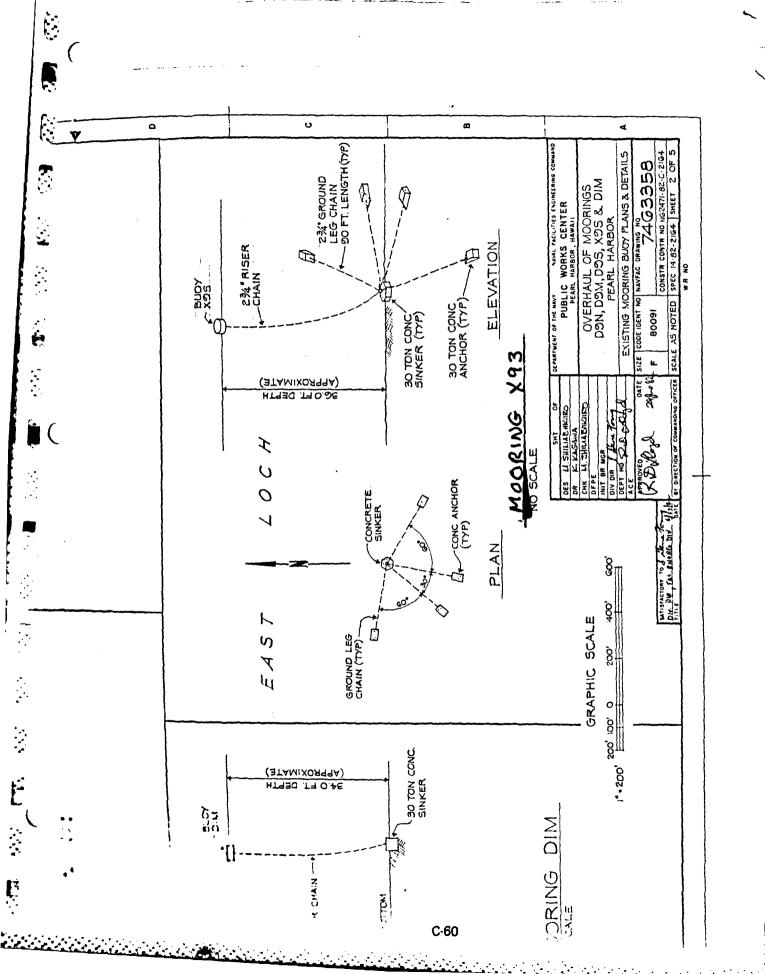
E

LAT. COORD. (N) =
$$22^{\circ}-22^{\circ}-48.0^{\circ}$$
 LONG. COORD. (W) = $157^{\circ}-57^{\circ}-16.5^{\circ}$

CHAIN SIZE =
$$2^{3/4}$$
.

ANCHOR 1 WT =
$$66,000$$
 # PADEYE SIZE = $2^{1/4}$ Department of $2^{3/4}$ ANCHOR 2 WT = $(50.)$ PADEYE SIZE = $(50.)$ PADEYE SIZE = $(50.)$ PADEYE SIZE = $(50.)$ PADEYE SIZE = $(50.)$

(x) four graded to class & after 1979 W/ Insp.



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6-86